

1 An Elevated Load-Bearing Platform

2 [Cross Reference](#)

US6173922	22. Apr. 1997	16. Jan. 2001	Robert P. Hoyt	Failure resistant multiline tether
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4 [Background of the Invention](#)

5 These teachings relate generally to a structure for supporting facilities, such as
6 habitable floor space, space vehicle launch and recovery systems, and related
7 support systems, at altitudes that are higher than can typically be reached
8 using compressive structures such as buildings and towers. These teachings
9 also relate to methods for erecting and maintaining said structure.

10 Currently, altitudes above the limited reach of towers, buildings, and aircraft
11 are accessed using systems based on rocket propelled vehicles. These systems
12 generally employ a multitude of different sub-systems to complete a round trip
13 journey. For example, launch gantries and multiple thruster stages will typically
14 be used for achieving orbit. Variants sometimes substitute an early rocket stage
15 with a stage that uses air breathing engines. Aero-braking systems, such as
16 ablative shielding, various parachutes, as well as more rockets, wings, and
17 landing gear may be used during a return journey.

18 Some components of these systems experience extensive wear during their use.
19 In practice, component recovery and refurbishment can be costly - so costly in
20 fact that abandoning used components and replacing them with new ones is
21 often economical. Therefore, these systems tend to have high operational costs.

22 The vehicles used typically subject their passengers and payloads to significant
23 stress, shake, and vibration. They are not considered to be as safe or as reliable
24 as commercial terrestrial transportation systems.

25 Many people are surprised that the cost of an "everyday object", such as a pen
26 or a toilet, is significantly inflated when that object is designed to be used in
27 space. Rocket based systems tend to make the cost and weight of *the payload*
28 *itself* higher. Payloads need to be engineered to be stronger to withstand the

29 stresses of launch, and this can make them heavier or costlier. When the
30 payload is a passenger, the passenger typically needs extensive training and
31 medical examination. Because the aforementioned costs are high, the
32 verification costs associated with preparing payloads is also high, as it would
33 not be acceptable for the payload to reach its destination and then fail to
34 operate properly – or die, in the case of living payload or a passenger.

35 Years of developmental effort and substantial funding have been invested into
36 this field by the military, research administrations, and commercial enterprises
37 of several economically successful countries. Many variations and
38 improvements on rocket propelled vehicle concepts have been produced;
39 however, despite all the investment and effort, the complexity of these systems
40 remains high, and therefore the cost of using these systems remains high.

41 An advantage that rocket based systems do have over several large-scale fixed
42 infrastructure concepts, such as space elevators, is that they generally have a
43 low “non-recurring” or capital cost. This makes them a good choice for small
44 volumes of passengers and cargo. Similarly, a ferry can be a better choice than
45 a bridge when choosing the best transportation infrastructure for traversing a
46 certain body of water, provided that the demand for convenient passage across
47 that particular body of water is sufficiently small.

48 As demand for routine access to space grows, the analogy of “building a bridge”
49 becomes more attractive. Several ideas for “bridges” that can help our
50 civilization to migrate out into space have been incorporated into works of
51 speculative fiction or cited in the prior art. Those that are known to the inventor
52 include:

- 53 1) The Space Elevator
- 54 2) The Orbital Ring
- 55 3) The Space Fountain
- 56 4) The Launch Loop
- 57 5) Inflated Towers
- 58 6) Artificial Inflated Mountains

59 Each of these ideas faces unique challenges if applied to service current and
60 near-future demands of human civilization.

61 The Space Elevator concept is faced with at least some of the following
62 challenges:

- 63 1) High capital cost, if the main tether is built with commercially available
64 materials.
- 65 2) High cost to deploy the system using already established space access
66 infrastructure, namely rockets.
- 67 3) Vulnerability to impactors (such as space debris) and possibly elemental
68 oxygen.
- 69 4) The structure does not service a convenient destination for the purposes
70 of space tourism – tourists would spend too much of their vacation time
71 in transit.
- 72 5) During the journey to the destination (geosynchronous orbit) the elevator
73 car is exposed to space radiation; therefore, shielding material would be
74 needed to protect passengers and sensitive cargo. The weight of the
75 shielding material would add to the energy cost of making a trip up the
76 elevator.

77 The Orbital Ring concept is faced with at least some of the following challenges:

- 78 1) High capital cost of a minimally viable implementation. The main ring
79 circumference is greater than the circumference of Earth. The ring must
80 be massive and rigid enough to support the weight of at least one short
81 space elevator without distorting because of the concentrated load. Note
82 that as part of this concept, the small space elevator is attached to a
83 magnetically levitated carriage that travels around the ring opposite to
84 the direction of ring rotation. This allows the space elevator's tether to
85 remain in a constant position over the surface of the planet.
- 86 2) High cost to deploy the system. All of the ring's components would need
87 to be placed into orbit using our present space access infrastructure,
88 namely rockets. Alternately, the structure would have a dependency on a
89 non-existent infrastructure for mining materials and manufacturing

90 components in space. Establishing that infrastructure would, in turn, be
91 costly.

92 3) As a destination, it is a microgravity environment. This environment
93 would be uncomfortable for many tourists to endure. Their visits would
94 be short and thus a tourist industry would make less money. Workers
95 supporting the industry would experience loss of muscle mass and
96 reduced bone strength, and therefore they would need to be rotated out
97 more frequently.

98 4) The ring is somewhat exposed to space debris.

99 5) The ring is somewhat exposed to space radiation.

100 The Space Fountain concept is faced with at least some of the following
101 challenges:

102 1) It uses a high speed “mass stream” comprised of magnetically levitated
103 and accelerated pellets which travel at high speed through an evacuated
104 tube, making it a high-energy system. Energy is constantly being
105 converted from potential energy to kinetic energy and back again in order
106 to transfer static load forces from upper parts of the structure down to
107 the surface of the planet. The constant conversion of energy from one
108 form to another means that there is *flow* of energy. When energy flows,
109 there are associated energy losses. For example, energy may be lost due
110 to resistance in electrical wires, or inefficiencies in the magnetic systems
111 that accelerate and decelerate the pellets. The lost energy will generate
112 heat. Thermal dissipation systems will be needed to prevent overheating,
113 and the structure will need to support their additional weight. The pellets
114 themselves will convert energy into heat because eddy currents will be
115 created within the pellets as they pass through magnetic fields of varying
116 intensity during their journey through the evacuated tube. Therefore,
117 ultimately, the operational cost of providing replacement energy to a
118 space fountain may be quite high. This puts the technology into more
119 direct competition with rockets, which also have high operational costs.

- 120 2) Portions of the precision-guided mass stream are exposed to a variety of
121 terrestrial threats that could jar it or otherwise interfere with its smooth
122 operation, leading to catastrophic failure. These threats include seismic
123 events, lightning, strong winds, aberrant aircraft, small arms such as
124 portable missiles, rocket propelled grenades, gun-fire. A catastrophic
125 failure could cause the substantial energy of the mass stream to threaten
126 nearby establishments. This would likely increase regulatory hurdles for
127 securing approval to build the structure. Operational costs would also
128 increase if a condition of approval were that it had to be constructed
129 within a large secure zone that is enforced by a heavily patrolled
130 perimeter.
- 131 3) As much of the system's cross-sectional area is exposed to wind shear,
132 its top may sway. This could limit its utility for applications where
133 stability is required.
- 134 4) The per square foot cost to buy or lease high-altitude floorspace at the
135 top of a space fountain is expected to be very high. The floorspace would
136 therefore not be a suitable for sustaining large static loads, such as the
137 habitable facilities (restaurants, hotel rooms, entertainment venues, etc.)
138 that typically are desired by tourists. Therefore, it is unlikely that the
139 structure's capital and operational costs could be offset by leasing high-
140 altitude floorspace to a tourist industry.
- 141 5) The top of a single space fountain is not well adapted, geometrically, to
142 the problem of supporting a linear accelerator for accelerating space
143 vehicles horizontally to orbital velocities.

144 The Launch Loop concept is faced with at least some of the following
145 challenges:

- 146 1) See Space Fountain #1
- 147 2) See Space Fountain #2. Some proponents of this architecture recommend
148 that it be deployed off-shore, and near the equator, where the weather is
149 generally temperate. This would mitigate some kinds of terrestrial threats
150 but also expose it to new threats. For example, it might be difficult to

151 defend the underwater portions of the precision guided mass stream
152 from a torpedo attack or prevent accidental collision with a submarine
153 from ever occurring during the lifetime of the structure.

154 3) Some depictions of the Launch Loop in the literature suggest that the
155 precision guided mass-stream component can withstand the point force
156 loads, such as the point loads of the launched vehicles and the point
157 loads of individual guy wires, which are widely spaced. This suggests that
158 the precision guided mass-stream is designed to withstand these of point
159 force loads, but how this is achieved does not appear to be adequately
160 explained in the literature.

161 4) The procedure by which the structure is apparently erected adds
162 complexity to the design. The precision guided mass-stream would
163 experience more jostling and distortion during erection and startup than
164 during steady state operation. The engineering challenge of maintaining
165 vacuum along the considerable length of the structure is complicated by
166 the need for expansion joints. These expansion joints would also add
167 weight to the structure.

168 The Inflated Towers concept is faced with at least some of the following
169 challenges:

170 1) It shares challenges 3, 4, and 5 with the Space Fountain, namely loss of
171 stability due to exposure to wind shear, offering little useable floorspace
172 at the top, and not being well adapted to the job of supporting a long
173 linear accelerator for horizontally accelerating space vehicles up to orbital
174 velocities.

175 The Artificial Inflated Mountains concept is faced with at least some of the
176 following challenges:

177 1) Cost, including land cost and the cost of a staggeringly large number of
178 individual building "blocks" that are needed to construct it.
179 2) Environmental impact, as the mountain would likely disrupt the natural
180 habitat of everything underneath it. It would potentially interfere with

181 migration. It could increase fuel costs for air traffic that had to route
182 around it. And it could potentially affect the local climate.

183 [Summary of the Invention](#)

184 This invention relates generally to mechanisms for supporting facilities at a
185 distance from a planetary body, such as the planet Earth, and more specifically
186 to supporting facilities at a high altitude above the surface, and if desired at a
187 fixed position relative to the surface.

188 The facilities may include “plots” of habitable floor space that can be leased to
189 help recoup costs, such as attractions, accommodations, and services for a
190 tourist industry. Other facilities may serve space industries by winching
191 passengers and cargo from the surface to a high altitude, and then accelerating
192 them tangential to the planetary body to reduce the cost of orbital insertion.

193 The invention utilizes a precision guided mass stream to generate a useful lift
194 force and this makes it an active structure; however, it has several critical
195 advantages over other proposed active structures. First, the invention teaches
196 how distortion and circuitous redirection of the mass stream may be reduced
197 relative to prior art both during construction and during steady state operation,
198 which in turn reduces the complexity and increases the reliability of the mass
199 stream. Once erected, the invention allows *the entire* mass stream to be placed
200 at an altitude where it is relatively defensible against both terrestrial threats
201 and space threats. It can be positioned well above the reach of most weapons of
202 war, commercial air traffic, weather, and seismic events yet still close enough to
203 the planet to receive the protection that the residual atmosphere offers against
204 space debris and meteorites.

205 The remaining atmosphere, planetary magnetic fields, and mass of the planet
206 will help to shield inhabitants from exposure to solar and space radiation. The
207 altitude of the structure can be selected and adjusted to optimize for more or
208 less natural shielding versus other benefits, such as the quality of the views, the
209 amount of air resistance experienced by accelerated vehicles, and overall cost
210 and complexity.

211 **Brief Description of the Drawings**

212 FIG. 1 is an orthographic projection of the planet Earth showing how the
213 invention might be deployed such that it encircles the continent of Antarctica.
214 The inset diagram shows a close-up of a section of the invention.

215 FIG. 2a and FIG. 2b are cut-a-way close-up views of a portion of the apparatus
216 that show a portion of the lift stay supported high-speed electromagnetic
217 bearing in proximity to a planet and details of the bearing's interior.

218 The FIG. 2a view shows a perspective where the planet 201 is seen side-on with
219 its north pole at the top, the bearing is encircling Antarctica (as was depicted in
220 FIG. 1), and the view is zoomed-in on the left side of the apparatus.

221 FIG. 2b is the same view as FIG. 2a but with the image is rotated clockwise by
222 about 140°. In this view, the surface of the planet 201 is horizontal. The figure
223 shows what the apparatus would look like from the point of view of an observer
224 standing on the surface of the planet.

225 FIG. 3 is a flow chart showing phases of construction and deployment for a
226 preferred embodiment.

227 FIG. 4 is a cut-a-way view that depicts a preferred embodiment of the invention
228 within an encasement system during early construction and testing.

229 FIG. 5 is a cut-a-way view that depicts a preferred embodiment of the invention
230 within an encasement system during later construction and testing.

231 FIG. 6 is a perspective drawing that depicts a few facilities supported by a
232 section of the bearing.

233 FIG. 7 is a three-dimensional rendering of the apparatus showing the bearing
234 encircling the planet and being supported above the planet's surface by a
235 plurality of forked lift stays.

236 FIG. 8a is a top-view and a side-view of a standard ball bearing with an inset to
237 show a close-up of the left side of the side-view.

238 FIG. 8b is a top-view and a side-view of a magnetic bearing of similar
239 dimensions to the ball bearing of FIG 8a, but much smaller in diameter than the
240 magnetic bearing of FIG. 1, FIG. 2, FIG. 4, and FIG. 5. The inset shows a close-
241 up of the left side of the side-view of the bearing.

242 Detailed Description of the Invention

243 In FIG. 1, an orthographic projection of the planetary body 101 (The Earth),
244 shows a portion of the southern hemisphere and the continent of Antarctica.
245 The invention comprises at least one bearing 102 deployed around the
246 continent. The detail view of FIG. 1 shows the invention's at least one lift stay
247 103. In the preferred embodiment, the at least one lift stay 103 is a branched
248 stay so that it can distribute its tensile force across many attachment points at
249 the bearing 102 end, while being thicker and more robust at the end that is
250 anchored to the surface at anchor points located on the protruding side of the
251 planetary body 101. If the planet were defined as having two "sides" relative to
252 the plane of the bearing 102, then the protruding side of the planet is the
253 volumetrically smaller side. In FIG. 1 this is the side that includes the continent
254 of Antarctica.

255 For the embodiment depicted in FIG. 1, the axis of rotation of the rotating part
256 of the at least one bearing 102 is approximately the same as the axis of
257 rotation of the planet. Other embodiments, where the axis of rotation of the
258 bearing is different from the planet's axis of rotation, are also possible.

259 In FIG. 2, a cut-a-way view of the southerly latitude of a planetary body 201 is
260 shown as a thick solid line arc, and the edge of space 202 is shown as a dotted
261 line arc to provide a rough sense of the overall scale. If the planet were Earth,
262 then the edge of space 202 may best be defined as the Kármán line. The at
263 least one bearing 203 is represented by a small circle, not drawn to scale. This
264 circle represents a point where the at least one bearing 203 intersects with the
265 plane of the cut-a-way view. To help the reader understand the positional
266 relationship of the entire at least one bearing 203 and the at least one lift stay
267 204, more of the at least one bearing 203 is shown in faint gray as it fades into
268 the distance, curves around and disappears behind the planetary body 201 and

269 also as it comes into the foreground, and again curves around and passes in
270 front of the planetary body 201. These off-the-plane-of-the-figure portions of
271 the at least one bearing are labeled 209. However additional lift stays for
272 supporting these additional portions 209 are not shown, as they would
273 excessively clutter the figure.

274 FIG. 2 depicts the mechanics for a discrete portion of the invention, where a
275 discrete portion is a portion of reasonably small size. If one were setting up a
276 calculus problem in a cylindrical coordinate space, one would typically use a
277 'd θ ' term (in addition to 'r' and 'z') and then solve by integrating over all values
278 of θ from 0 to 2π . Similarly, a discrete portion represents a portion wherein the
279 use of a d θ term in a mathematical description might be considered reasonable.

280 The at least one lift stay 204 is shown in the drawing stretching between the at
281 least one bearing 203 and the at least one anchor point 205 on the surface of
282 the planet 201. Note that the at least one lift stay's 204 curvature is
283 approximated in this illustration, and that the at least one anchor point 205
284 may be an off-shore platform that is itself secured to the bottom of the ocean
285 by cables or other means known in the art of off-shore platform design.

286 The dotted line arrow 206 represents the force of gravity acting on a unit length
287 segment of the at least one bearing 203 and its supported payload (not shown
288 in FIG. 2). The dotted line arrow 207 represents the inertial force that is
289 generated predominantly by the at least one bearing's at least one rotating ring
290 211 for a unit length segment of the at least one bearing. Note that the non-
291 rotating parts of the at least one bearing 203 and its payload may technically be
292 moving as well because the planet is rotating and this may contribute slightly to
293 the overall inertial force vector 207. The dotted line arrow 208 represents a
294 tensile force that the at least one lift stay 204 will exert on a unit length
295 segment of the at least one bearing 203. When it is the operator's intent for a
296 unit length segment of the at least one bearing 203 and its payload to remain
297 at a fixed position, these three force vectors 206, 207 and 208 will be adjusted
298 by the operator so that they are substantially in equilibrium. In said equilibrium,

299 the gravity force vector **206** is countered by the inertial force vector **207** and
300 the tensile force vector **208** exerted by the at least one lift stay **204**.

301 It is preferred that an appropriate equilibrium is maintained for all unit length
302 segments of the at least one bearing **203** and that the nature of the equilibrium
303 is continuous and relatively unchanging between adjacent unit length
304 segments. Uniform distribution of the forces exerted by the payload(s) and the
305 at least one lift stay **204** on the at least one bearing **203** is also preferred. It
306 should be apparent to one skilled in the art, that the stronger the construction
307 of the at least one bearing **203** is, the more it will be able to tolerate localized
308 non-uniformity in the distribution of forces acting upon it. Analogously, the
309 stiffness of a suspension bridge allows it to tolerate a certain amount of non-
310 uniform loading as vehicles of differing weight travel across it.

311 Inside the at least one protective casing **210** of the at least one bearing **203**
312 there is at least one rotating ring **211**. At least one non-rotating ring **212** is
313 shown inside the at least one protective casing **210** as well, and the at least one
314 non-rotating ring **212** is attached to the at least one lift stay **204**, **215** through
315 the wall of at least one protective casing **210**. The at least one protective casing
316 **210** serves to isolate the interior components from matter in the surrounding
317 environment which could generate heat, increase friction, or otherwise interfere
318 with the optimal operation of the interior components.

319 FIG. 8a and FIG. 8b provide some context and help to explain why the at least
320 one bearing **203** was so named. FIG. 8a shows a standard mechanical ball
321 bearing, albeit one with an unusually large outer diameter to band width ratio.
322 FIG. 8b shows a similarly sized magnetic bearing. As is well known to one
323 skilled in the art of magnetic bearings, the positional relationship between an
324 active magnetic bearing's stator and its rotor are maintained by using sensors,
325 electromagnets, and controllers.

326 The ball bearing of FIG. 8a would fall apart if its diameter were to be increased
327 several thousand-fold; however, the magnetic bearing of FIG 8b would not fall
328 apart (if properly designed) because the magnetic coupling technique is less
329 reliant on the structural stiffness of the ring material. A magnetic bearing

330 maintains the positional relationship between its inner and outer rings by
331 dynamically adjusting the forces of its coupling mechanism 213 and 214;
332 therefore, there is no practical upper limit on the diameter of such a magnetic
333 bearing. Because a magnetic bearing does not rely on balls rolling in tracks, its
334 maximum speed and operational life can be designed to greatly exceed that of
335 a ball bearing.

336 In the preferred embodiment, air is evacuated from within the at least one
337 protective casing 210 so that the moving parts of the at least one bearing 203
338 will not lose a significant amount of energy due to air friction. Too much lost
339 energy would increase the operational cost of maintaining the at least one
340 rotating ring's 211 speed. It would also increase the cost and complexity of
341 thermal dissipation systems for managing waste heat.

342 Rings are coupled by a coupling mechanism 213, 214. The coupling mechanism
343 uses, for example, properties of electromagnetism to generate forces of
344 attraction and/or repulsion between the at least one rotating ring 211 and the
345 at least one non-rotating ring 212. These forces are applied to maintain the
346 positions of the rings with respect to one another within the tolerances
347 supported by the coupling mechanism, even while at the at least one rotating
348 ring 211 and the at least one non-rotating ring 212 are in motion relative to
349 one another. In the preferred embodiment the coupling mechanism 213, 214 is
350 designed to impart minimal friction and generate minimal waste heat. This
351 ensures that the operational cost of maintaining the at least one rotating ring's
352 211 rate of rotation is manageable and the cost and complexity of thermal
353 dissipation systems for managing waste heat is likewise reasonable. In order to
354 minimize magnetically induced friction, the preferred embodiment's at least
355 one rotating ring 211 will be as unvarying as possible from the perspective of
356 the at least one non-rotating ring 212 in the vicinity of the coupling
357 mechanism. Likewise, the preferred embodiment's at least one non-rotating
358 ring 212 will appear to be as unvarying as possible from the perspective of the
359 at least one rotating ring 211 in the vicinity of the coupling mechanism.

360 To better understand the meaning of “as unvarying as possible”, some
361 examples of undesirable variations may be illustrative. If a plurality of individual
362 coupling mechanism components were to be spaced at discrete intervals, such
363 that the magnetic flux density experienced by a ring was stronger near a
364 coupling mechanism component than it was in between adjacent coupling
365 mechanism components, this would represent an undesirable variation. If the
366 coupling mechanism generated a magnetic flux within a ring and the properties
367 or geometry of the ring in the vicinity of the magnetic flux changed periodically
368 due to, for example, the presence of expansion joints, this would be another
369 example of an undesirable variation. While it is seen as advantageous for
370 manufacturing reasons for a ring to be made up of many discrete elements, it is
371 preferred that these discrete elements be designed so that they integrate
372 together seamlessly. If the magnetic field in the vicinity of a non-uniformity
373 were different from the magnetic field elsewhere, then this magnetic field
374 difference would travel rapidly around one ring from the perspective of the
375 other. At any given point, a magnetic field difference that passes by would be
376 perceived as a *changing* magnetic field. Changing magnetic fields can cause
377 current to flow and this can lead to energy losses. The preferred embodiment
378 will strive to avoid such losses by adhering sufficiently to these mutual
379 uniformity requirements. It should be noted that there are other methods
380 known in the art for avoiding such losses, such as using laminates of
381 conductive paramagnetic material and insulators to minimize the size of eddy
382 current loops. The preferred embodiment would make judicious use of eddy
383 current loop minimizing techniques as well.

384 Note that it is anticipated that the at least one protective casing **210** and the at
385 least one non-rotating ring **212** could be blended together into a single
386 component that serves the purposes attributed to both components in these
387 teachings. Alternately the at least one non-rotating ring **212** as well as sub-
388 components of the coupling mechanism **213, 214** could be outside the
389 protective casing **210** to make them more accessible and thus easier to service.
390 The use of separate components (that is, the at least one non-rotating ring
391 **212**, the protective casing **210**, and the coupling mechanism **213, 214**) has

392 been chosen to help facilitate the illustration and explanation of technical
393 concepts.

394 The coupling mechanism 213, 214 is also designed to be able to increase,
395 decrease, and maintain the at least one rotating ring's 211 rate of rotation.
396 Conversion of electrical energy to and from kinetic energy through the use of,
397 for example, electromotive forces, is well known in the art. Electric motors,
398 generators, and linear motors routinely perform such conversions. In the
399 preferred embodiment, the coupling mechanism 213, 214 is able to overcome
400 any forms residual friction (magnetic, air, or other) within the at least one
401 bearing 203 and increase the at least one rotating ring's 211 rate of rotation up
402 to the level required to generate the inertial forces needed for the invention to
403 operate. In the preferred embodiment the coupling mechanism is a single
404 system that serves two purposes: 1) maintaining the ring's 211, 212 positions
405 in relation to one another, and 2) adjusting the rate of ring rotation. However, it
406 is anticipated that these two purposes could also be served by two separate
407 systems (e.g. a coupling system and an electromotive system).

408 Within the detail view of FIG. 2, the at least one rotating ring 211 and at least
409 one non-rotating ring 212 are depicted as having a slight angle relative to the
410 inertial force vector 207. This angle occurs because gravity acts upon the at
411 least one rotating ring 211. Thus, to keep the rotating ring's path of travel in
412 position, the coupling mechanism must, on average, generate at least one
413 steady force vector that is at an angle with respect to the inertial force vector
414 207. For the depicted coupling mechanism 213, 214, the at least one force (not
415 shown) is an attractive force. This allows the coupling mechanism to
416 substantially counter both the combined inertial force vector 207 and the
417 gravity force vector 206 acting on the mass of the rotating ring using at least
418 one roughly equal and opposite attractive force. With this slight angle, the need
419 for the coupling mechanism 213, 214 to counter an additional constant
420 shearing forces, relative to each other, is reduced; therefore, the figure
421 represents a preferred embodiment where, in the absence of outside

422 disturbances, the steady force would, at least momentarily, be in equilibrium
423 with the other forces.

424 If the steady force were generated, for example, using only the attractive
425 properties of paramagnetic materials, then Earnshaw's theorem would suggest
426 that the system would not be stable. However, it is well known to one skilled in
427 the art of magnetic levitation or active magnetic bearings that in practice stable
428 magnetic levitation is possible despite Earnshaw's theorem. It is achievable by
429 employing servomechanisms, supportive diamagnetic materials, or
430 superconductors, for example. It is anticipated that within the coupling
431 mechanism 213, 214, there is at least one additional control force that will
432 work in conjunction with the at least one attractive force to maintain the ring
433 positions with respect to one another, within design tolerances, in the presence
434 of reasonable external perturbations and despite any inherent instability
435 associated with the generation of the at least one steady force.

436 Furthermore, it is anticipated that the bearing would be designed so that the at
437 least one slight angle would be adjustable, using, for example, a system of
438 servos (not shown). At the anticipated scale of a preferred embodiment, the at
439 least one bearing's 203 components will not experience significant mechanical
440 stress if each at least one angle is uniformly adjusted and relatively consistent
441 around the entire bearing. This angular adjustment would permit each of the at
442 least one steady forces to be directed as needed. Adjustment of its direction
443 and magnitude will be needed, for example, when the bearing is raised or
444 lowered, or when the bearing's payload is increased or decreased.

445 It should be noted that an alternate embodiment is envisioned where the at
446 least one rotating ring 211 and the at least one non-rotating ring 212 are
447 repositioned such that maintaining their relative position requires at least one
448 roughly equal and opposite *repulsive* force, in addition to various controlling
449 forces. Analogously, some maglev train technologies are known to lift the train
450 using attractive forces and others lift the train using repulsive forces.

451 In practice, the bearing may be initially constructed and at least partially tested
452 at a first location, and then deployed at a second location. For example, the

453 first location could be on or slightly below the planet's surface or on or slightly
454 below the surface of its hydrosphere. Deploying the bearing to a second
455 location will likely require that it rise up to an operational altitude. By adjusting
456 the force vectors (206, 207, and 208) to be slightly out of equilibrium, a
457 resultant acceleration can be generated. It is preferred that force adjustments
458 be made so that the acceleration is perpendicular to the inertial force vector
459 207, otherwise the acceleration would cause the bearing's circumference to
460 change. Excessive circumference change could buckle the at least one bearing
461 203 or generate excessive or unwanted circumferential stress within it.

462 If, for example, the at least one bearing 203 is initially constructed so that it is
463 centered around and perpendicular to the planet's axis of rotation (this is the
464 case in the depictions of both FIG. 1 and FIG. 2) then the resultant acceleration
465 would preferably be configured to cause the bearing to accelerate slowly *along*
466 the planet's axis of rotation in the direction that would take it away from the
467 planet's surface. This direction would be towards the bottom of FIG. 2a. In the
468 cylindrical coordinate system defined by 'r', ' θ ', and 'z', centered on the
469 planet's axis of rotation, the motion would be along the 'z' axis. Similarly, the
470 forces would be preferably adjusted to make the resultant acceleration act to
471 decelerate the at least one bearing 203 as it nears its operational altitude. The
472 forces can also be manipulated to accelerate the at least one bearing 203 back
473 towards the planet's surface and bring it to a gentle stop as it nears the
474 surface.

475 The at least one bearing 203, or portions of it, can also be accelerated and
476 decelerated, if needed, to avoid asteroids or space debris that are detected to
477 be on a collision trajectory. In these circumstances, small amounts of bearing
478 circumference change, or changes along the 'r' axis, in addition to changes
479 along the 'z' axis, may be considered acceptable for the sake of expediency.

480 There are several ways that forces may be adjusted. The amount of inertial
481 force may be adjusted by changing the rotational speed of the at least one
482 bearing's 203 at least one rotating ring 211. (Note: the symbol 219 indicates
483 that, in this cross-section, the direction of motion of the least one rotating ring

484 211 is into the page.) The tensile forces exerted by the at least one lift stay 204
485 may be adjusted by tensioning using a spooling mechanism to winch the stay,
486 by moving the at least one anchor point 205 across the surface of the planet,
487 by adding or removing (if there were previously a plurality of lift stays 204) at
488 least one lift stay 204, and by any other means familiar to one skilled in the art
489 of adjusting tensile forces within cables or fibers. The gravity force vector 206
490 may be adjusted by adding, removing, or redistributing the mass of, or the
491 mass supported by, the at least one bearing 203. The at least one bearing 203
492 may exert a circumferential force by tightening or loosening if it is designed to
493 expand or contract, or if it naturally expands or contracts due to weather
494 conditions and seasonally varying amounts of direct heating by sunlight.
495 Methods to achieve expansion or contraction include heating or cooling,
496 mechanically generating compressive or tensile forces using actuators such as
497 pistons, using electromagnetism (including interaction with the planet's
498 magnetic field), a mechanical drive system, bio-engineered muscle,
499 piezoelectric actuators, material expansion due to absorption, or any other
500 technique that is useful for generating tensile or compressive forces that is
501 familiar to one skilled in the art of generating forces within materials,
502 machines, or structures. The circumferential force is not shown as it is
503 considered to be a small force on a planetary scale implementation of the
504 invention, however it may be a relevant and useful force in a smaller scale
505 implementation of the invention, such as a prototype implementation.

506 The at least one bearing 203 and the plurality of lift stays 204 may incorporate
507 navigational aids, such as lights, radio transponders, and tracking systems to
508 assist with guiding ships and air traffic in the vicinity.

509 FIG. 3 is a flowchart that describes a process of constructing and erecting the
510 preferred embodiment.

511 For the preferred embodiment, construction begins with the fabrication of parts
512 on the planet. Then the parts will be loaded onto ships, assembled, and
513 deployed such that they are just under the surface of the ocean, such that the
514 completed bearing encircles Antarctica. The ability to initially deploy the

515 structure in the ocean is advantageous because it potentially reduces property
516 acquisition, right-of-way, and environmental challenges. There are also fewer
517 natural and manmade obstacles in the ocean than on land. This is a major
518 reason for proposing a southerly location for the preferred embodiment. It is
519 also advantageous for the bearing to maintain a stationary position over the
520 Earth without experiencing gyroscopic forces associated with the Earth's
521 rotation, so in the preferred embodiment the structure is positioned such that
522 the at least one rotating ring's axis of rotation is substantially parallel to the
523 planet's axis of rotation. A design wherein the bearing's approximate center is
524 offset with respect to the planet's axis of rotation is also anticipated. Such a
525 design affords the invention the ability to support facilities at a variety of
526 different altitudes. For example, the altitudes optimal for tourism facilities may
527 be different from the altitudes that are optimal for facilities that launch
528 payloads into space. Note that the at least one bearing 203 does not have to be
529 a perfect circle as at the scale of the invention the at least one bearing 203
530 would be somewhat flexible.

531 The construction depth in the ocean may be selected to be low enough to avoid
532 ships and icebergs, but not so deep that the engineering cost of withstanding
533 water pressure and operations costs of working at the selected depth is too
534 high. Technology and equipment that today are used to lay large undersea oil
535 pipelines may be repurposed for this phase of the project.

536 FIG.4, not to scale, depicts an earlier phase of construction. During this phase,
537 the bearing is enclosed within an encasement system 401 so that it would be
538 protected from the ocean and yet still accessible for inspection and outfitting
539 purposes. While safely underwater, the at least one moving bearing 411 and the
540 coupling mechanisms 413, 414 could be tested within their protective casing
541 410 at gradually greater and greater speeds until sufficient margins of safety at
542 operational speeds have been established. In the event of catastrophic failure
543 during underwater testing, the surrounding ocean would decelerate fast moving
544 fragments so they would not be ejected from the vicinity of the construction
545 site at high speeds. The partial vacuum of near space could be recreated inside

546 the encasement system **401** so that testing conditions would be as realistic as
547 possible. Testing could include, for example, firing projectiles from a high
548 energy cannon (not shown) at various components to establish the design's
549 resilience to micro-meter impact, and the ability of various automated repair
550 systems (not shown) to work quickly and reliably to make repairs in a near-
551 vacuum environment.

552 The vacuum containment system, instrumentation, emergency backup systems,
553 automated repair systems, etc. could all be verified during this phase of
554 construction.

555 To prevent the inertial forces from stretching the bearing during testing, at
556 least one temporary construction stay **404 & 405** would be attached between
557 the outer shell of the encasement system **401** and at least one temporary
558 construction stay anchor point on the planet's lithosphere **406**. The buoyancy
559 of the encasement system **401** and the anchoring effect of the at least one
560 temporary construction stay **404 & 405** must be designed to work together to
561 prevent the bearing from drifting around during construction and testing. To
562 provide additional stability, actuators **402** will actively maintain the position of
563 the bearing **410** relative to the planet within required tolerances, so long as the
564 position of the encasement system **401** relative to the planet is stable within
565 somewhat looser tolerances. It is anticipated that at least one thruster nacelle
566 (not shown) affixed to the exterior of the encasement system may be employed
567 to assist with positioning efforts and/or to serve as a backup stability system.

568 FIG. 5, not to scale, depicts a later phase of construction. After initial testing
569 has completed, the process of deploying the at least one bearing **510** to its
570 operational altitude can begin. Shipping and icebergs will need to be directed
571 away from the encasement system **501** for this phase. The at least one
572 temporary construction stay **504 & 505** could be loosened to allow the
573 encasement system **501** to float to the surface. The at least one lift stay **515**
574 will be affixed to the at least on bearing **510**. The at least one bearing's **510** at
575 least one rotating ring **511** will be accelerated to an operational rotational
576 speed. The inertial force vector **207** of the bearing **203** would combine with the

577 tensile force vector **208** provided by the at least one lift stay **204** and the
578 gravity force vector **206** acting on the bearing **510**. (Note that referring to the
579 forces depicted in FIG 2 is somewhat misleading in this context as FIG. 2 shows
580 the invention in an already deployed state.) The rotational rate (and thus inertial
581 force) would be adjusted, and the at least one lift stay **515** would be tensioned,
582 so as produce resultant acceleration of the at least one bearing **510** parallel to
583 the planetary body's axis of rotation, and away from the planet. However, the
584 resultant acceleration will not yet move the bearing **510** away from the planet's
585 surface as it is still held in position by the anchored encasement system **501**.
586 As mentioned earlier, it is preferred that the resultant acceleration should be
587 parallel to the planet's axis of rotation to prevent hoop stresses (not shown)
588 that would cause the bearing's circumference to increase or decrease.

589 The top of the encasement system **501** could be removed and the telescoping
590 actuators **502** could position the bearing sufficiently clear of the surface to
591 allow facilities and other systems to be added. During the outfitting phase, the
592 load on the bearing should be evenly distributed at a fairly constant level.

593 With outfitting completed, the bearing would be released from the telescoping
594 actuators **502** and raised to higher altitudes by maintaining the right balance of
595 inertial and tensile forces while gradually unwinding the at least one lift stay
596 **515** from at least one spool mounted on an ocean going vessel while
597 simultaneously moving the at least one spool on the vessel towards the planet's
598 pole, and away from the bearing. In the preferred embodiment, the at least one
599 lift stay **515** will always be either safely wrapped around the at least one spool
600 or it will be under tension and in use to help support the bearing. It would not
601 be desirable for a lift stay **515** to rest on the ground or float in the ocean at any
602 point during construction.

603 From the point of view of someone on one of the ocean-going vessels, this
604 phase of the process would be somewhat analogous to a child launching a kite.
605 Typically, the kite's string starts out mostly wound on a spool, and is gradually
606 unwound as the kite gains altitude. Often the child will move backwards away
607 from the kite as he/she unwinds the string. In the case of the preferred

608 embodiment, the inertial forces generated within the at least one bearing 510
609 are analogous to the wind force that serves to tension the kite's string, the
610 ocean-going vessel is analogous to the child, and the at least one lift stay 515
611 is analogous to the kite's string. In the preferred embodiment there are, of
612 course, a plurality of lift stays 515 and ocean-going vessels operating in a
613 precisely coordinated manner using advanced navigational aids to accomplish
614 the goal of raising the bearing to its operation altitude.

615 FIG. 7 shows how the deployed bearing 702 and lift stays 703 may appear to an
616 observer who is orbiting the planet 701.

617 Referring back to FIG. 2, when the bearing has been raised to its operational
618 altitude, the anchor end of the at least one lift stay 204 can be transferred from
619 the ocean-going vessel to an anchor 205. The at least one anchor relative to
620 the planetary body 205 in the preferred embodiment would also have the ability
621 to adjust the tension of the lift stay 204, and it would be designed to withstand
622 and/or repel terrestrial threats, including storms, tsunamis, weapons typically
623 available to terrorists, collisions with ocean vessels and aircraft, etc. The at
624 least one anchor 205 could also be a tall structure. This would add some
625 additional altitude to the overall invention and help ensure that the low end of
626 the at least one lift stay 204 was more difficult to reach and thus damage from
627 the surface of the planet. For example, if the anchor 205 was a 500m tall
628 structure, and the at least one lift stay 204 were attached to the top of it, then
629 it would be more difficult for a terrorist in a boat to strike the lift stay 204
630 using, for example, a Rocket Propelled Grenade (RPG).

631 It is also preferable for the at least one anchor 205 to be repositionable, ideally
632 under its own power. This capability would be needed, for example, in the
633 event that an ice sheet was to break away from the planet's ice cap and drift
634 towards the at least one anchor 205. The anchor could then be repositioned to
635 be out of the path of the drifting ice sheet while simultaneously maintaining
636 tension on the at least one lift stay 204. If a very large ice sheet remained intact
637 while being on a collision course with at least one anchor 205 (as opposed to
638 breaking apart naturally) then it might become necessary to accelerate the ice

639 sheet's break up using explosives. This would enable the at least one anchor
640 **205** to travel in and around smaller ice sheet fragments. It might also be
641 necessary to temporarily lower the operational altitude of the at least one
642 bearing **203** to increase engineering safety margins during these operations.

643 FIG. 6 shows a section of the at least one bearing **600** supporting at least one
644 payload winching system facility **601** and at least one domicile facility **602**, **603**
645 via at least one tie **604**. At least one transportation system facility provides a
646 means of accelerating at least one vehicle **607** along at least one track **605** that
647 is, for example, supported by at least one arm **606** attached to at least one
648 payload winching system facility **601** or at least one domicile facility **602**, **603**.
649 Stops may be made at various facilities to load or offload passengers and cargo
650 through at least one doorway **611**, **612**. Note that the at least one payload
651 winching system facility **601**, the at least one domicile facility **602**, **603**, and the
652 at least one vehicle **607** preferably incorporate some habitable enclosures. The
653 at least one doorway **611**, **612** is preferably a pressure sealed doorway that
654 provides access to habitable enclosures. The at least one transportation system
655 may alternately be attached directly to the at least one bearing **600** or to at
656 least one of the at least one lift stays (not shown in FIG. 6).

657 The at least one transportation system may optionally be fully or partially
658 enclosed within a tube (not shown). A fully enclosed tube may be a sealed tube
659 and the environment within that tube may differ from the environment outside.
660 For example, the environment within may be more evacuated to further reduce
661 air friction, or it may be less evacuated so that it can sustain human life in case
662 a vehicle's pressure containment system fails. A partially enclosed tube may
663 serve to attenuate the sound of passing vehicles so as not to disturb residents
664 of the at least one facility.

665 The at least one transportation system (or at least one transportation system
666 specially purposed for space vehicle launch and recovery) may accelerate the at
667 least one vehicle **607** to a suitable orbital or space travel speed at which point a
668 mechanism for releasing vehicles **608** and **609** is activated to release the at
669 least one vehicle **607**. A similar launch and recovery facility could be used to

670 accelerate a recovery vehicle (the recovery vehicle would not detach from the
671 track) up to a speed that would enable it to rendezvous with a space vehicle
672 that was returning to the planet from space. The space vehicle could maneuver
673 so that it would momentarily match its velocity and position with the moving
674 recovery vehicle, such that it could be retrieved, using at least one grapppler (not
675 shown), by the recovery vehicle. Once linked, the recovery vehicle could
676 decelerate the space vehicle so that passengers and cargo could exit the space
677 vehicle and enter one of the supported facilities. Alternately, passengers and
678 cargo could simply enter the recovery vehicle through an airlock. In this way the
679 space vehicle, its cargo, and its passengers would be spared the hardship and
680 perils of returning to the planet's surface using aero-braking techniques. It
681 would also be less costly to refurbish the space vehicle and return it to service,
682 relative to other vehicles that are designed to travel to and from the surface of a
683 planet with an atmosphere, such as The Space Shuttle system developed by
684 NASA.

685 Passengers and cargo may travel between the surface and the at least one
686 bearing **600** via at least one cable **610**. A facility that supports a form of
687 transport that uses at least one cable **610** is referred to as a payload winching
688 system **601**.

689 Note that FIG. 6 is a greatly simplified depiction of the bearing **600** supporting
690 various facilities and domiciles as well as an inter-facility transportation
691 system. The inventor anticipates that in practice the transportation system
692 would comprise sufficient tracks to provide service in both directions and to
693 allow individual vehicles to accelerate and decelerate so that they can travel
694 while merged into a stream of vehicular traffic.

695 With respect to the payload winching system **601**, it should be pointed out that
696 one skilled in the art of moving passengers or cargo vertically knows that any of
697 a number of different techniques may be employed. For example, a cable can
698 be spooled on a powered drum, a cable can wind around a powered drum and
699 then connect to a counterweight, a cable can loop around a powered drum at

700 one end and a pulley at the other, and a cable can be stationary but the car can
701 grip the cable in a manner that allows it to climb the cable.

702 In the preferred embodiment, the stationary cable technique is used with at
703 least two cables. The cable is a tapered cable made from an available material
704 of high specific strength, such as carbon fiber. The car is equipped with a
705 mechanism that allows it to grip the cable and climb it rapidly without causing
706 the cable to experience wear at an unacceptable rate. Stabilizers positioned at
707 points along the length of the cable serve to keep the cable at a stationary
708 position in the presence of wind using aeronautical techniques. Stabilizers are
709 designed so that they will not obstruct the passage of an elevator car. For
710 example, a stabilizer can be long and it can attach to the cable at multiple
711 points. This way individual attachment points can temporarily detach one at a
712 time to allow the car to pass by unimpeded.

713 The stabilizers draw AC electrical power inductively from insulated wires within
714 the cable. Within each cable embedded insulated wires of finite length overlap
715 with one another to generate inter-wire capacitance. This capacitance allows
716 the individual wires to AC couple, which allows an AC current to travel along the
717 entire length of the cable, while simultaneously preventing a significant DC
718 current from travelling further than the finite length of one of the individual
719 embedded wires. This prevents the cable from becoming a path-of-least-
720 resistance for built up charges in the atmosphere to discharge through.

721 To reduce the amount of power loss through electromagnetic radiation, the at
722 least two cables form a differential pair and the AC current in one is made to be
723 always equal and opposite to the AC current in the other. If more than two
724 cables are used, then a multi-phase AC current can be transmitted that is
725 designed to achieve the same minimal aggregate AC current effect. The
726 stabilizers separate the cables and inductively couple with each cable
727 individually to draw power.

728 The car itself will be equipped with stabilizing technology such as gyroscopes
729 and thrust systems so that passengers will experience a smooth ride even on

730 windy days. It also draws power inductively from the embedded wires within the
731 cables like the stabilizers do.

732 The planetary body **101** may be any moon, planet, or celestial object that the
733 invention is anchored to.

734 A bearing may be comprised of more than two rings and the rings may all have
735 different rotational rates. A bearing comprised of many nested rings where the
736 rates vary incrementally from ring to adjacent ring is covered by this invention
737 and is seen as a design variant that potentially allows for maximum speed
738 differential between an outermost and innermost ring while there is a smaller
739 speed differential between any two adjacent rings. This may be an
740 advantageous variant for maintenance or friction reduction purposes.

741 It is anticipated that embodiments of the invention may, in practice, comprise
742 more than one bearing to provide redundancy in case of failure and so that
743 individual bearings can be taken out of service occasionally for maintenance
744 and repair.

745 A typical ball bearing relies on the mechanical rigidity of its rings to create a
746 track that balls or rollers can roll in. As the at least one bearing **203** in the
747 claimed apparatus is large, mechanical rigidity of its rings is not sufficient to
748 maintain their positional relationship with respect to one another. The bearings
749 rings are therefore held together by other means. The preferred means is to use
750 a coupling mechanism **213, 214** which employs electrically controlled magnetic
751 forces to maintain the spacing of the rings with respect to one another. A
752 plurality of sensors will measure the spacing between adjacent rings and feed
753 their measurements into a control function. The control function will adjust the
754 magnetic forces in response to the measurements in order to maintain the
755 desired spacing. It is preferred that the target spacing between rings **211, 212**
756 of the at least one bearing **203** be at a distance where the magnetic fields
757 generated by permanent magnets will provide exactly the right amount of force
758 to counter the differences in centripetal forces between two rings **211, 212**.
759 Electrically generated alterations of the magnetic force would then only be

760 needed for control purposes to make corrections if portions of the rings at least
761 one **211**, **212** drift from the optimal position relative to one another.

762 The preferred embodiment's at least one coupling mechanism **213**, **214** uses at
763 least one first force that does not consume power and at least one second force
764 that does consume power and is under the control of a controller. The first
765 force is the attractive or repulsive forces of permanent magnets, as described in
766 the preferred embodiment. It is anticipated that forces may be generated by
767 other means, such as by having charged particles traverse perpendicular to a
768 magnetic field (Lorenz forces), electrostatic forces, or using the magnetic flux
769 pinning properties of Type II superconductors. The second force can be
770 electrically generated magnetic fields, as described in the preferred
771 embodiment, or a mechanical force (hydraulics, pneumatics, motor,
772 piezoelectric device, or any other means known in the art of mechanical
773 actuation), or the adjustment of a charge across two-plates separated by a
774 distance or any other means known in the art for generating a controllable
775 force. In the case of a mechanically actuated second force, the second force
776 could control the position of at least one permanent magnet, for example, as a
777 means of controlling or maintaining the magnitude of the first force.

778 The at least one anchor **205** may be similar to an anchor used for the cables of
779 a suspension bridge. It could be connected directly to solid ground, such as
780 bedrock. However, it is also feasible to connect them to the planetary body
781 through machines that generate thrust by displacing the matter (e.g. in the
782 hydrosphere or atmosphere) of the planetary body. For example, an anchor
783 could be a ship that uses the thrust of its propellers to maintain its position in
784 the ocean and exert the correct amount of thrust on the anchored end of the at
785 least one lift stay **204**, or an aircraft that uses the thrust of its engines in the
786 atmosphere to exert a correct amount and direction of force on the anchored
787 end of the at least one lift stay **204**.

788 The at least one lift stay **204** could be a single cable; however, in the preferred
789 embodiment the lift stay **204** is designed so that it forks repeatedly so that
790 there are fewer anchor points near the planet's surface relative to the number

791 of attachment points at the at least one bearing **203**. Fanning-out a lift stay in
792 this manner enables one lift stay's arrays of attachment points to be overlapped
793 with the attachment points of an adjacent lift stay. This can provide redundancy
794 in case of individual lift stay failure. Fanning out also generates more evenly
795 distributed support at the bearing so that the bearing's protective casing **210**
796 would not need as much mechanical stiffness. At the other end of the lift stay
797 **204**, the fan-in leads to fewer obstructions and anchor points at the lower
798 altitudes. This makes it easier for air and sea traffic on routes near Antarctica to
799 navigate around the plurality of lift stays and anchors. It enables the lift stays to
800 be thicker and stronger at the lower altitudes, where they are more exposed to
801 terrestrial threats.

802 Individual lift stays may be angled so that they overlap in a crisscross fashion or
803 are interwoven in some manner. This would serve to provide rotational stability
804 to the at least one bearing **203**. It is anticipated that the techniques of
805 generative design could be used to explore numerous possible permutations,
806 given a set of design goals, to develop an optimized configuration for the
807 plurality of lift stays. It is not unusual for such design methodologies to
808 produce results that look almost organic in their construction. It is anticipated
809 that a plurality of lift stays **204** may be implemented as a regular or irregular
810 web or mesh of interconnected fibers.

811 The tensile force exerted by the plurality of lift stays **204**, when combined with
812 the inertial force of the at least one bearing **203**, counters the force of gravity.
813 When the plurality of lift stays **204** droops or sags less, more of its tensile force
814 **208** contributes to countering the force of gravity **206**, and less inertial force
815 **207** is needed to keep the three force vectors **206**, **207**, **208** in substantial
816 equilibrium. Sag can be minimized if the lift stay is very light in relation to its
817 strength, and that can be achieved by using high specific strength materials in
818 its construction. In the preferred embodiment, lift stays are engineered to take
819 advantage of both high specific strength materials, such as carbon fiber, and
820 also utilize the atmosphere for additional support. This will maximize the

821 gravity countering upward component of their force vector at the point where
822 they attach to the bearing.

823 Lift stay weight is affected by application of corrosion resistant coatings,
824 acoustic monitoring systems, and energy supply systems for automated repair
825 and maintenance machinery. Techniques such as acoustic monitoring
826 (essentially listening for snapping sounds with microphones positioned along
827 the length of the lift stay) are used to determine the location and frequency of
828 breaks that may occur in the individual strands of lift stay.

829 Our aeronautical industry has become very adept at reliably keeping all manner
830 of aircraft aloft in the skies above us. For example, the U-2 reconnaissance
831 aircraft, build in the 1950's, operates at an altitude of 70,000ft, or 21km above
832 sea level. It seems inevitable, therefore, that more optimal lift stay designs will
833 incorporate the science of airflow – and that considerable aeronautical
834 engineering expertise will be brought to bear on the problem of how to make
835 maximum use of it. Another relatively recent advance in the aeronautics
836 industry is in the field of automated aircraft, or “drones”. The use of a fleet of
837 drone aircraft 216 to shepherd the lift stays is seen as advantageous because
838 the drones can detach and return to base stations for maintenance or to other
839 facilities where they will be continually recycled and replaced. While attached,
840 for example by a short tether 217, to the lift stays they can draw power or fuel
841 from a lift stay borne power supply system as opposed to running on their own
842 internal power reserves.

843 As the winds and temperatures in the atmosphere vary, and as the bearing and
844 its lift stays cover vast distances, the means of advantageously incorporating
845 airflow into the design must be adaptable. For example, if the wind conditions
846 favor it, inflatable compartments 218 within the lift stays can be inflated with
847 hot air or hydrogen, so that they become light enough to be buoyed by the
848 atmosphere. If the wind is travelling along the lift stay, the lift stay could deploy
849 airfoils into the airflow to generate lift. If the wind is travelling across the lift
850 stay, the lift stay can be deflated and flattened into an airfoil itself. Propulsion
851 on the leading edge of the lift stay could pull the lift stay through the wind,

852 both keeping it straight and generating upward lift preventing the lift stay from
853 sagging under its own weight. Energy is needed to heat air, inflate or deflate
854 sections of the lift stay, or power propulsion systems, such as the
855 aforementioned attached drone aircraft.

856 Two methods are used in the preferred embodiment for delivering this energy:
857 1) deliver it electrically, and 2) deliver it by manufacturing hydrogen and
858 pumping that up the interior of the lift stay. It should be noted that there are
859 many methods of delivering energy that are well known in the art. Either or
860 both of the preferred methods may be considered depending on the
861 aeronautical engineering associated with the lift stay design at a given altitude.
862 Hydrogen plumbing might be lighter than electrical wiring and potentially
863 hydrogen fuel could more directly and efficiently fuel air heaters and engines.
864 Reserves of hydrogen stored inside the lift stay may have significantly better
865 energy density properties for this application than batteries. Thus, a hydrogen-
866 based design may be more resilient to interruptions in energy supply.

867 Hydrogen can also be readily converted to electricity using fuel cells; however,
868 the proponents of an electric design would no doubt point out that an
869 electrically powered design would be less flammable. Electric systems would
870 probably operate more reliably at higher altitudes where oxygen is scarce. The
871 best solution depends on factors that vary along the length of the lift stay. For
872 example, at extremely high altitudes the buoyancy of electrically heated
873 hydrogen is recommended and likely the most optimal solution. At lower
874 altitudes, electricity is recommended for powering propellers that generate
875 thrust.

876 While hydrogen will inevitably leak out through the walls of any container, if the
877 leaking hydrogen can be reacted with oxygen using a catalyst to generate
878 useful heat energy for increasing buoyancy, then non-permeable containment
879 of the gas does not need to become a requirement. Heat energy can be used to
880 generate more buoyancy from the hydrogen and to prevent ice from building
881 up on the lift stays, and to prevent the materials from becoming fragile and
882 cracking if exposed to extreme cold.

883 If support of lift stays were lost, then the bearing would start to fall back
884 towards the planetary body. If a risk analysis deemed it necessary, then the
885 bearing could be equipped with a safety system, such as parachutes (if the lift
886 stays themselves are insufficient), retro-rockets, air bags, or some other
887 means, to lower its terminal velocity and cushion its impact with the ocean.

888 Winching is the action of moving cargo away from the surface of a planetary
889 body and towards the bearing and moving cargo away from the ring towards
890 the surface of a planetary body.

891 Cargo includes vehicles or containers containing provisions, equipment,
892 supplies, materials, people, biologics, goods, waste or anything else that needs
893 to be transported.

894 The preferred embodiment for the system for accelerating vehicles is a maglev
895 system. Maglev systems are well known in the art and maglev technology is
896 currently used in some modern transportation systems on Earth.

897 The preferred embodiment for the system that releases vehicles is at least one
898 electromagnet coupled to a ferromagnetic plate that would be turned off in
899 order to release the vehicle. The magnet could have a mechanical grapppler as a
900 back-up system or for parking purposes when the vehicle needs to be fully
901 powered down.

902 A habitable compartment comprises systems that support some human
903 necessities such as breathing adequately pressurized air, drinking water,
904 temperature control, and as a means to enter and exit the compartment. The
905 cabin of an airplane is an example of a habitable compartment.

906

907 What is claimed is:

- 908 1) (Currently amended) An apparatus for elevating at least one facility above
909 the surface of a planetary body, wherein the apparatus comprises at least
910 one bearing where the circumference of said at least one bearing is
911 smaller than the circumference of said planetary body and yet large
912 enough to completely encircle a portion of said planetary body, and a
913 plurality of lift stays connected between said at least one bearing and at
914 least one anchor point positioned on a protruding side of said planetary
915 body, where:
- 916 a. For at least one discrete portion of the at least one bearing, a
917 tensile force vector generated by at least one lift stay combines
918 through a coupling mechanism with an inertial force vector
919 produced by at least one rotating ring to generate a resultant force
920 vector that acts in opposition to the downward force of gravity,
 - 921 b. For said at least one discrete portion of the at least one bearing,
922 neither said tensile force vector nor said inertial force vector on
923 their own act in direct opposition to the downward force of gravity.
- 924 2) (Currently amended) The apparatus of claim 1 where the at least one
925 bearing's uses at least one coupling mechanism that utilizes magnetic
926 forces to maintain a positional relationship between at least one rotating
927 ring and at least one non-rotating ring.
- 928 3) (Currently amended) The apparatus of claim 2 where the at least one
929 bearing uses at least one electromotive system to increase or decrease
930 the rotational rate of at least one rotating ring.
- 931 4) (Currently amended) The apparatus of claim 2 where the at least one
932 rotating ring is inside at least one protective casing.
- 933 5) (Currently amended) The apparatus of claim 4 where a vacuum is
934 maintained within the at least one protective casing.
- 935 6) (Currently amended) The apparatus of claim 2 where the at least one
936 rotating ring is engineered to have an unvarying effect on magnetic flux
937 from the perspective of the at least one non-rotating ring in the vicinity
938 of non-electromotive parts of the coupling mechanism.

- 939 7) (Currently amended) The apparatus of claim 2 where the at least one
940 non-rotating ring is as engineered to have an unvarying effect on
941 magnetic flux from the perspective of the at least one rotating ring in the
942 vicinity of non-electromotive parts of the coupling mechanism.
- 943 8) (Currently amended) The apparatus of claim 1 where no part of the
944 bearing rests upon or within the hydrosphere or lithosphere of a
945 planetary body or is otherwise supported via transference of compressive
946 forces through a strut, tower, or other supporting structure that is in turn
947 supported by the hydrosphere or lithosphere of said planetary body.
- 948 9) (Currently amended) The apparatus of claim 1 where the at least one
949 facility is a facility for transporting vehicles containing passengers or
950 payloads around the circumference of the bearing to and from various
951 other facilities.
- 952 10) (Currently amended) The apparatus of claim 1 where the at least
953 one facility is a launch facility for accelerating at least one vehicle along
954 the at least one bearing and where said facility is configured to release
955 said vehicle from said facility to enable said vehicle to reach its final
956 destination using less propellant than would be needed relative to
957 launching said vehicle from the surface of the planetary body.
- 958 11) (Currently amended) The apparatus of claim 1 where the apparatus
959 comprises at least one payload winching system.
- 960 12) (Currently amended) The apparatus of claim 1 where the apparatus
961 is configured to elevate at least one permanent and habitable facility.
- 962 13) (Currently amended) The apparatus of claim 1 where the at least
963 one lift stay is a forked lift stay.
- 964 14) (Currently amended) The apparatus of claim 1 where at least one of
965 a plurality of compartments within or attached to at least one of the
966 plurality of lift stays may be:
- 967 a. Inflated with a lighter than air gas so that said lift stay's droop can
968 be reduced using the buoyancy of said lighter than air gas when
969 low wind speeds permit the lift stay to have a larger cross-section,
970 and

- 971 b. Deflated when having a smaller cross-section to the wind is
972 preferable because it will make it easier to keep the lift stay on
973 station.
- 974 15) (Currently amended) The apparatus of claim 1 where the cross-
975 sectional shape of at least a portion of at least one of the plurality of lift
976 stays is re-configurable to optimize the flow of air passing by said lift
977 stay due to wind.
- 978 16) (Currently amended) The apparatus of claim 1 where a plurality of
979 drone aircraft serves to maintain the position of at least one of the
980 plurality of lift stays and where the drone aircraft can draw power from at
981 least one of the plurality of lift stays.
- 982 17) (Currently amended) The apparatus of claim 1 where at least one of
983 the plurality of lift stays is connected to at least one anchor that is
984 repositionable.

985

986 [Abstract of the Disclosure](#)

987 An apparatus is described for supporting payloads at high elevations with
988 respect to a planetary body. The apparatus comprises a bearing that encircles a
989 portion of a planetary body. One ring of the bearing rotates, and a coupling
990 mechanism transfers centripetal forces to another non-rotating ring. Lift stays
991 connect the non-rotating ring to the planetary body; and contribute a force that
992 is in equilibrium with the centripetal and gravitational forces. A preferred
993 embodiment is constructed and tested in the ocean and then raised to altitude.
994 Its coupling mechanism employs magnetic forces and its lift stays are
995 interwoven, partially supported and stabilized aeronautically, and anchored to
996 the planet. The apparatus's elevation is not supported by transferring forces to
997 the surface through the inertia of precision-guided high velocity components,
998 thus these components are not necessarily exposed to seismic activity, weather,
999 or anomalous air traffic.